

# Frequency Response Techniques using Bode and Nyquist Plots

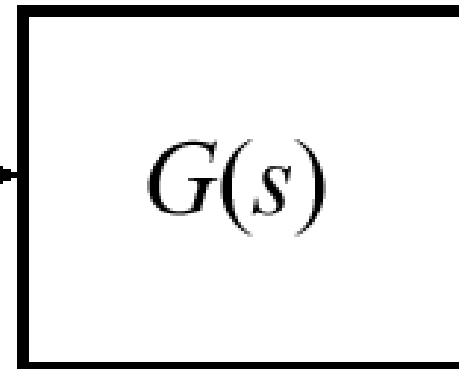
# Concept of Frequency Response

**Input  $\sin(\omega t)$**

**System**

**Response**

$$R(s) = \frac{\omega}{s^2 + \omega^2}$$



$C(s)$

# Concept of Frequency Response

$$C(s) = \frac{\omega}{s^2 + \omega^2} G(s)$$

$$= \frac{K_1}{(s + j\omega)} + \frac{K_2}{(s - j\omega)} + \textit{Fraction terms for } G(s)$$

**Forced**

**Steady-state**

**Natural**

**Dies out**

# Concept of Frequency Response

$$K_1 = \frac{\omega}{(s - j\omega)} G(s) \Big|_{s=-j\omega} = \frac{1}{2} jG(-j\omega) = \frac{1}{2} M_G e^{-j(\phi_G - \pi/2)},$$
$$K_2 = \frac{\omega}{(s + j\omega)} G(s) \Big|_{s=j\omega} = -\frac{1}{2} jG(j\omega) = \frac{1}{2} M_G e^{j(\phi_G - \pi/2)}$$

**where**  $M_G = |G(j\omega)|$   
 $\phi_G = \text{angle of } G(j\omega)$

# Concept of Frequency Response

$$C_{ss}(s) = \frac{K_1}{(s + j\omega)} + \frac{K_2}{(s - j\omega)}$$

$$= \frac{1}{2} M_G \left[ \frac{e^{-j(\phi_G - \pi/2)}}{(s + j\omega)} + \frac{e^{j(\phi_G - \pi/2)}}{(s - j\omega)} \right]$$



$$c_{ss}(t) = \frac{1}{2} M_G \left[ e^{-j(\omega t + \phi_G - \pi/2)} + e^{j(\omega t + \phi_G - \pi/2)} \right]$$

$$= M_G \sin(\omega t + \phi_G)$$

# Concept of Frequency Response

**Input**

**System**

**Response**



$$R(t) = \sin(\omega t) \quad \rightarrow \quad c(t) = M_G \sin(\omega t + \phi_G)$$

**where**  $M_G = |G(j\omega)|$  &  $\phi_G = \text{angle of } G(j\omega)$

# Concept of Frequency Response

## System Parameters

- Magnitude  $M_G = |G(j\omega)|$
- Phase angle  $\phi_G = \text{angle of } G(j\omega)$

## System Representation

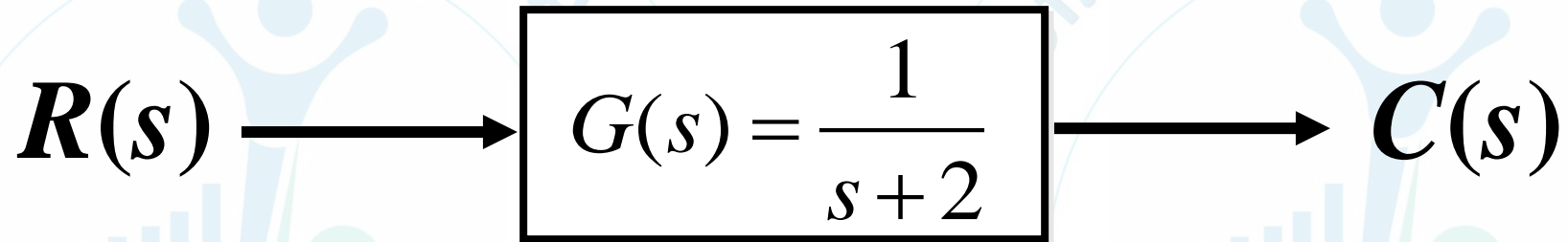
**Bode Diagram**  $M_G$  &  $\phi_G$  vs.  $\omega$

**Nyquist Diagram**  $M_G$  vs.  $\phi_G$  for  $0 < \omega < \infty$



# Concept of Frequency Response

## Example 10.1



$$G(j\omega) = \frac{1}{j\omega + 2} = \frac{2 - j\omega}{\omega^2 + 4} = M_G e^{j\phi_G}$$

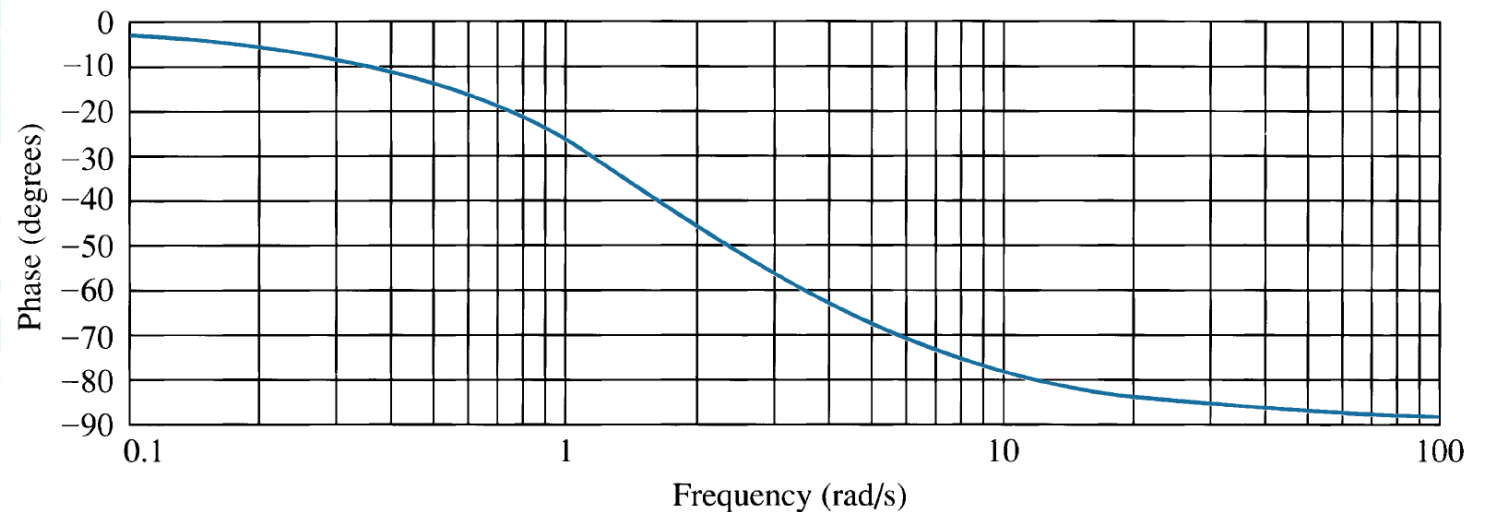
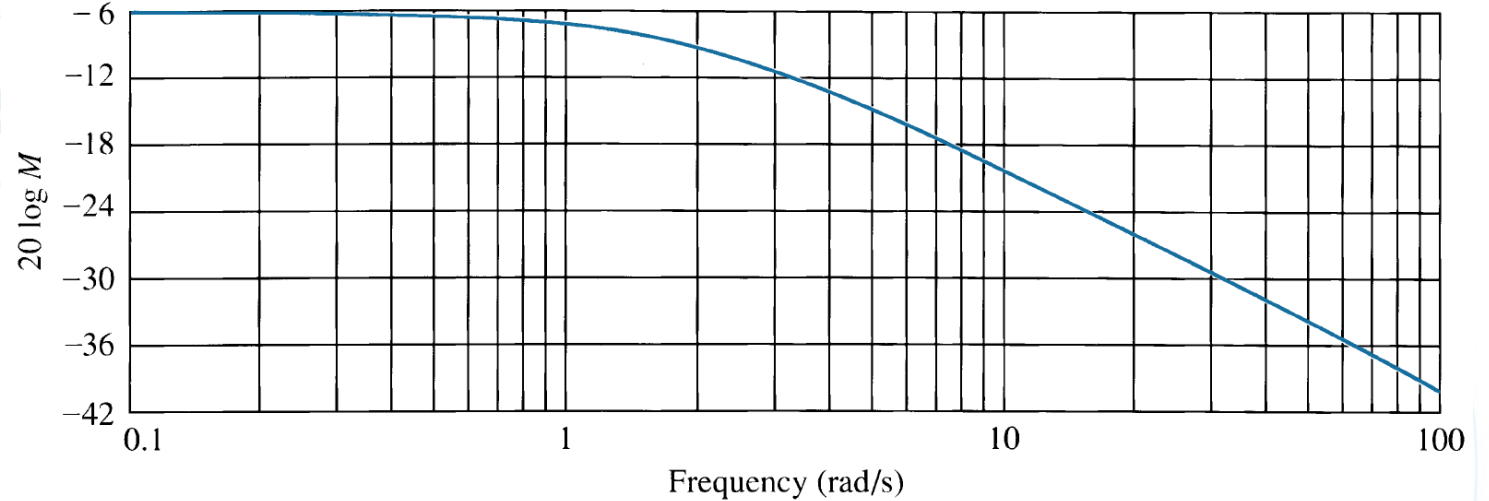
$$\rightarrow M_G = \frac{1}{\sqrt{\omega^2 + 4}}, \quad \text{and} \quad \phi_G = -\tan^{-1}\left(\frac{\omega}{2}\right)$$



# Concept of Frequency Response

## Example 10.1

### Bode Diagram



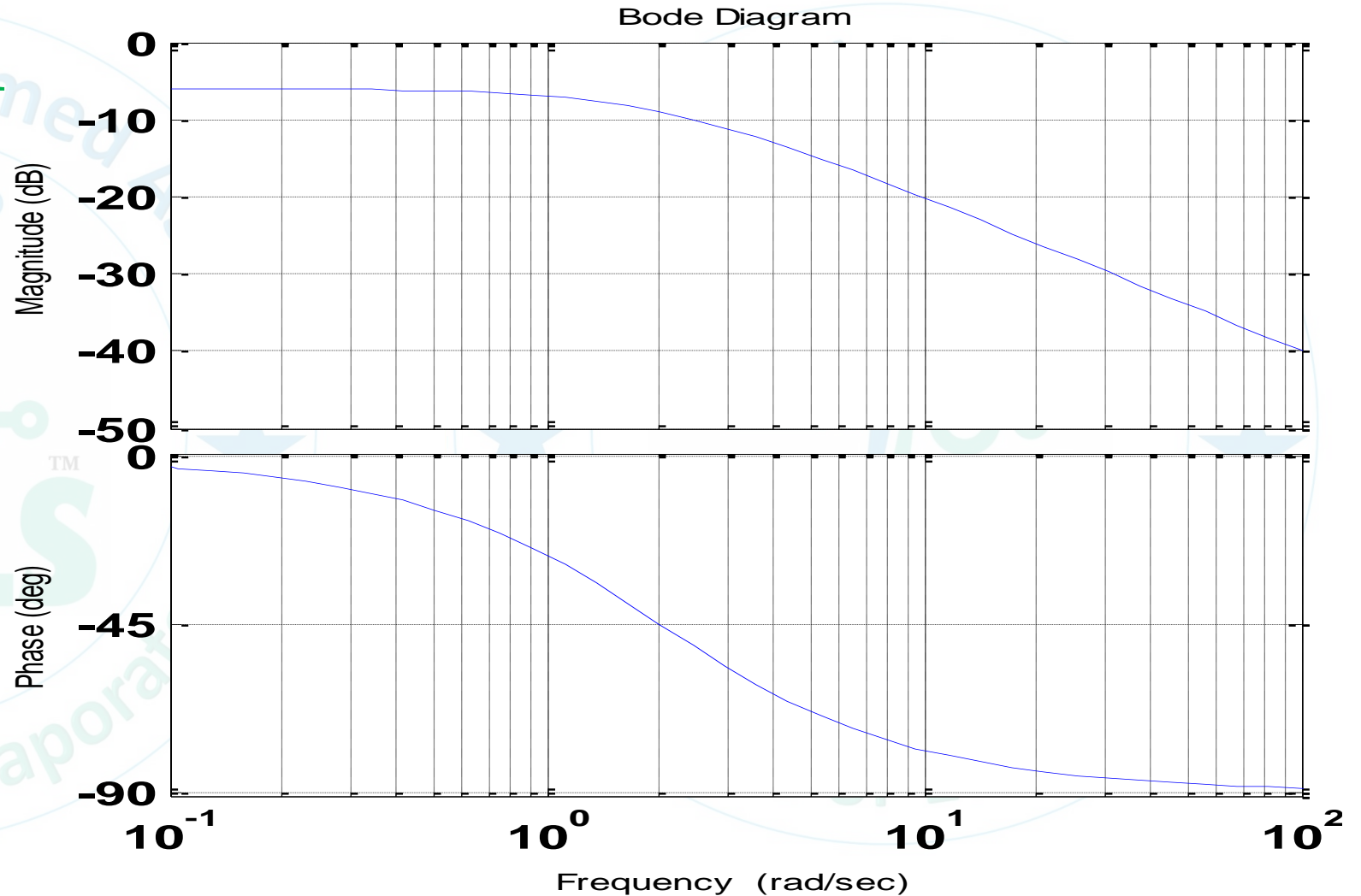
# Frequency Response using Bode Plot

## Example 10.1

```
>> n=1;  
>> d=[1 2];  
>> bode(n,d)  
>> grid
```

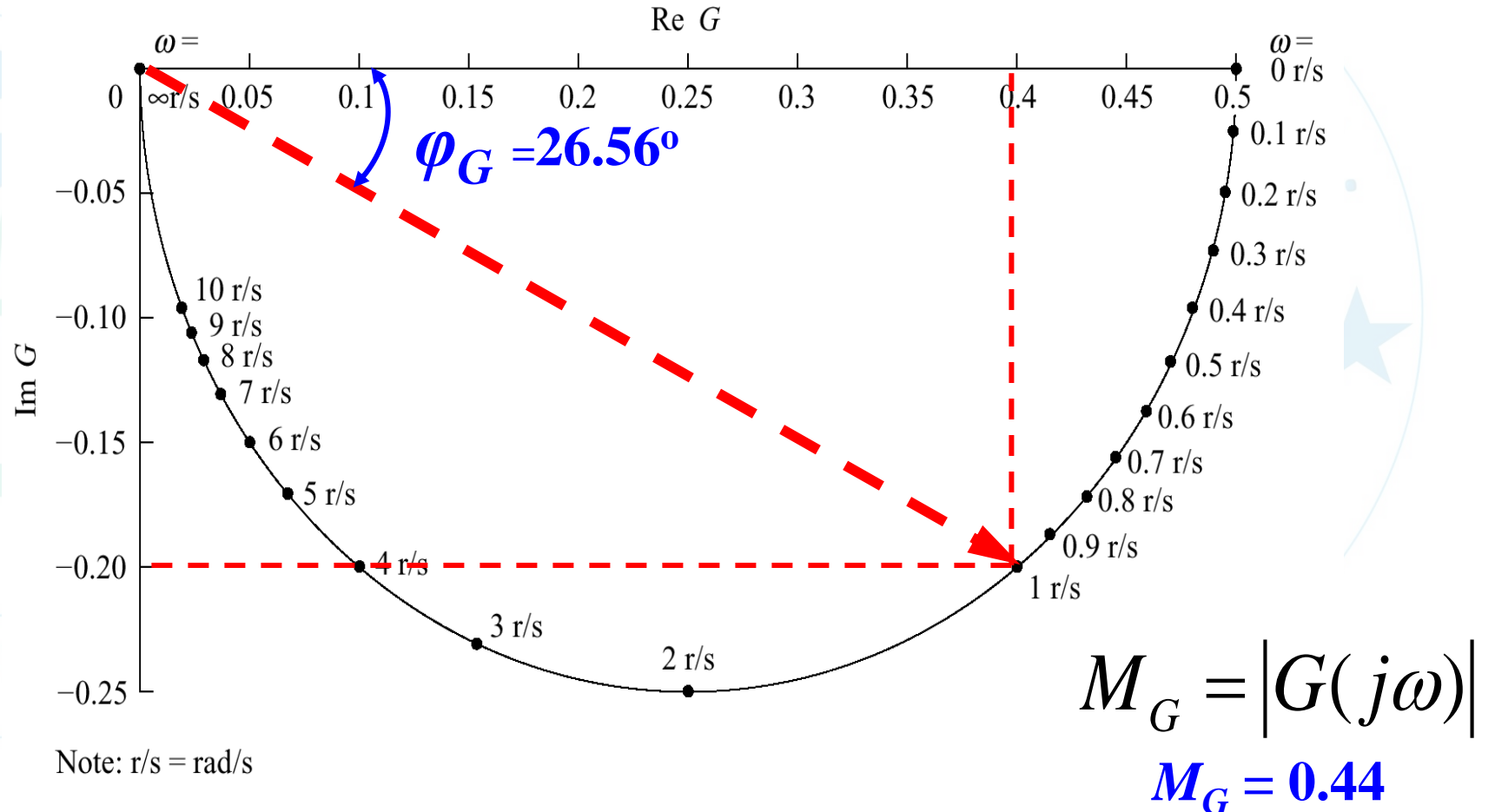


Hendrik Bode  
1905 -1982



# Frequency Response using Nyquist Plot

## Example 10.1



# Frequency Response using Nyquist Plot

## Example 10.1

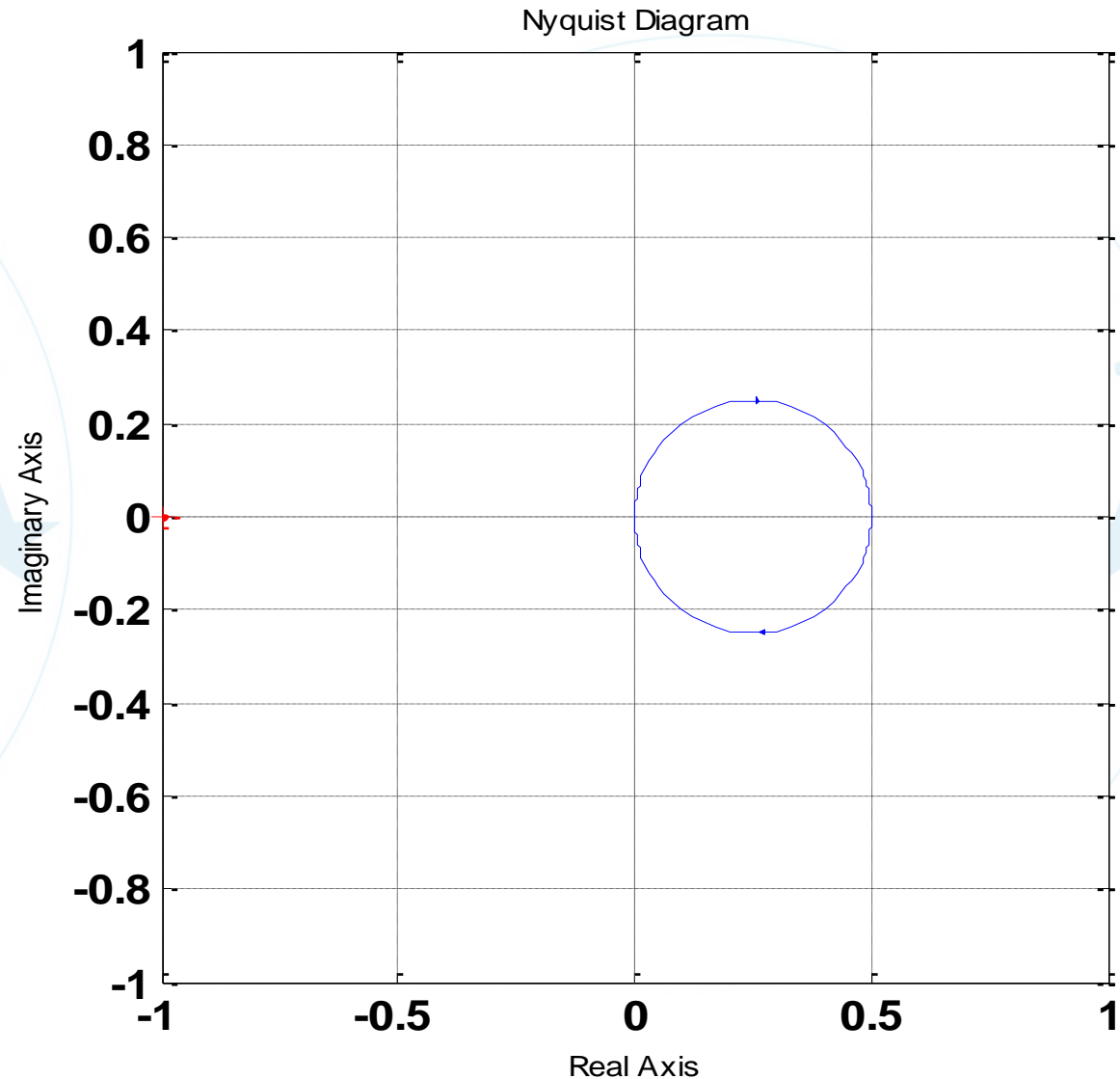
```
>> n=1;  
>> d=[1 2];  
>> nyquist(n,d)
```



**Harry Nyquist**

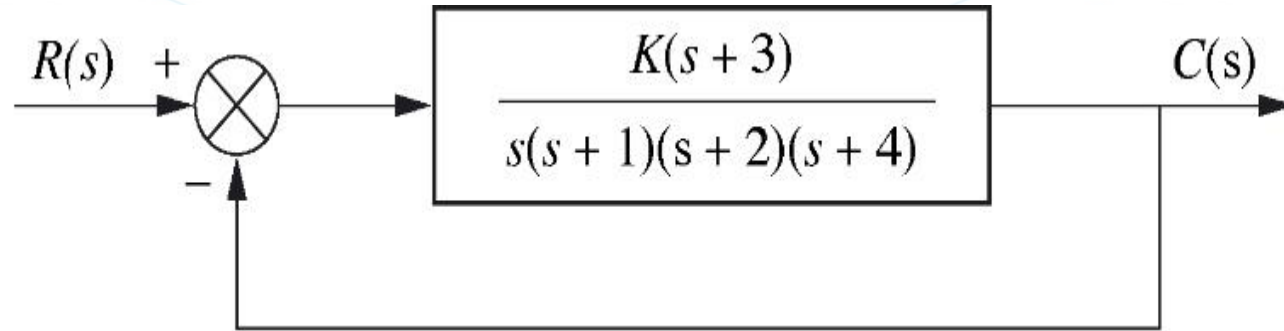
*b. Feb. 7, 1889, Nilsby, Sweden*

*d. April 4, 1976, Harlingen, Texas, U.S.*



# Nyquist Stability

Example



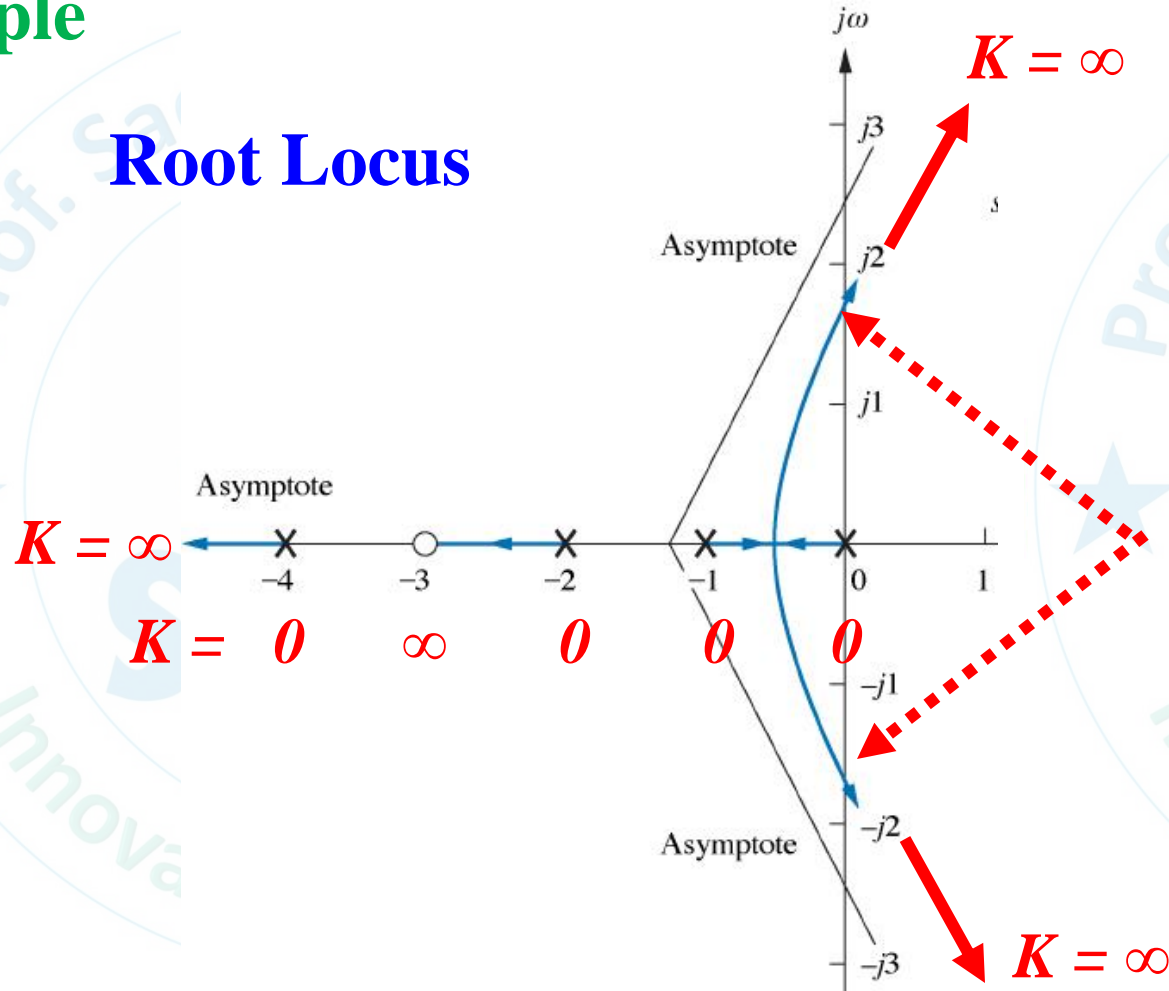
$$T = \frac{K(s+3)}{s^4 + 7s^3 + 14s^2 + (8+K)s + 3K}$$

$s^4$	1	14	$3K$
$s^3$	7	$8+K$	
$s^2$	$90-K$	$21K$	
$s^1$	$\frac{-K^2 - 65K + 720}{90-K}$		
$s^0$	$21K$		

# Nyquist Stability

## Example

### Root Locus



### From Routh Table

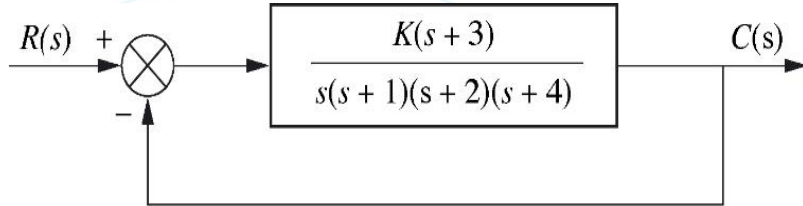
$$-K^2 - 65K + 720 = 0$$

$$\rightarrow K = 9.65$$



# Nyquist Stability

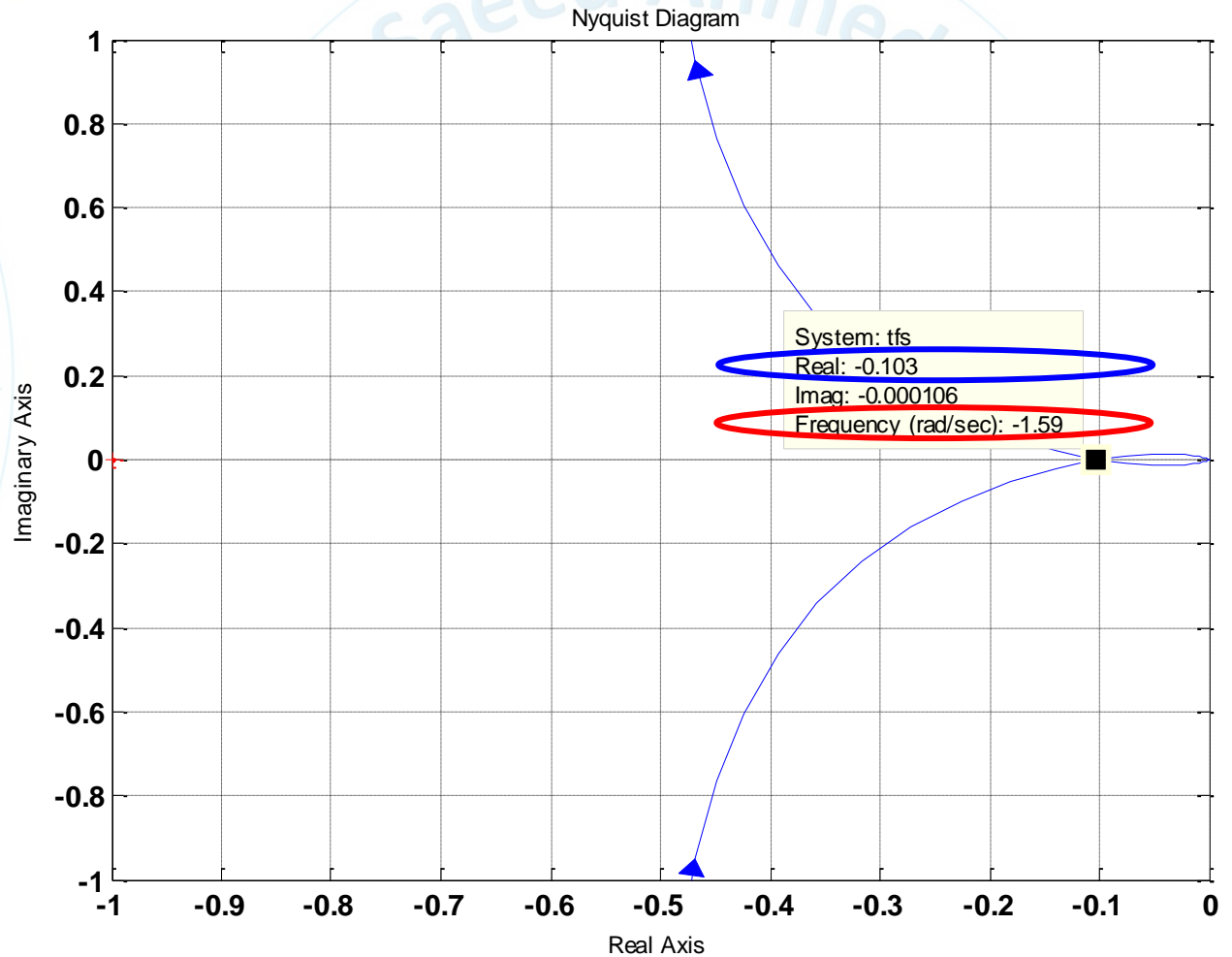
**Exmpl**



```
>> n=[1 3];
>> tfs=zpk([-3],[0 -1 -2 -4],1);
>> nyquist(tfs)
```

**Gain Margin**

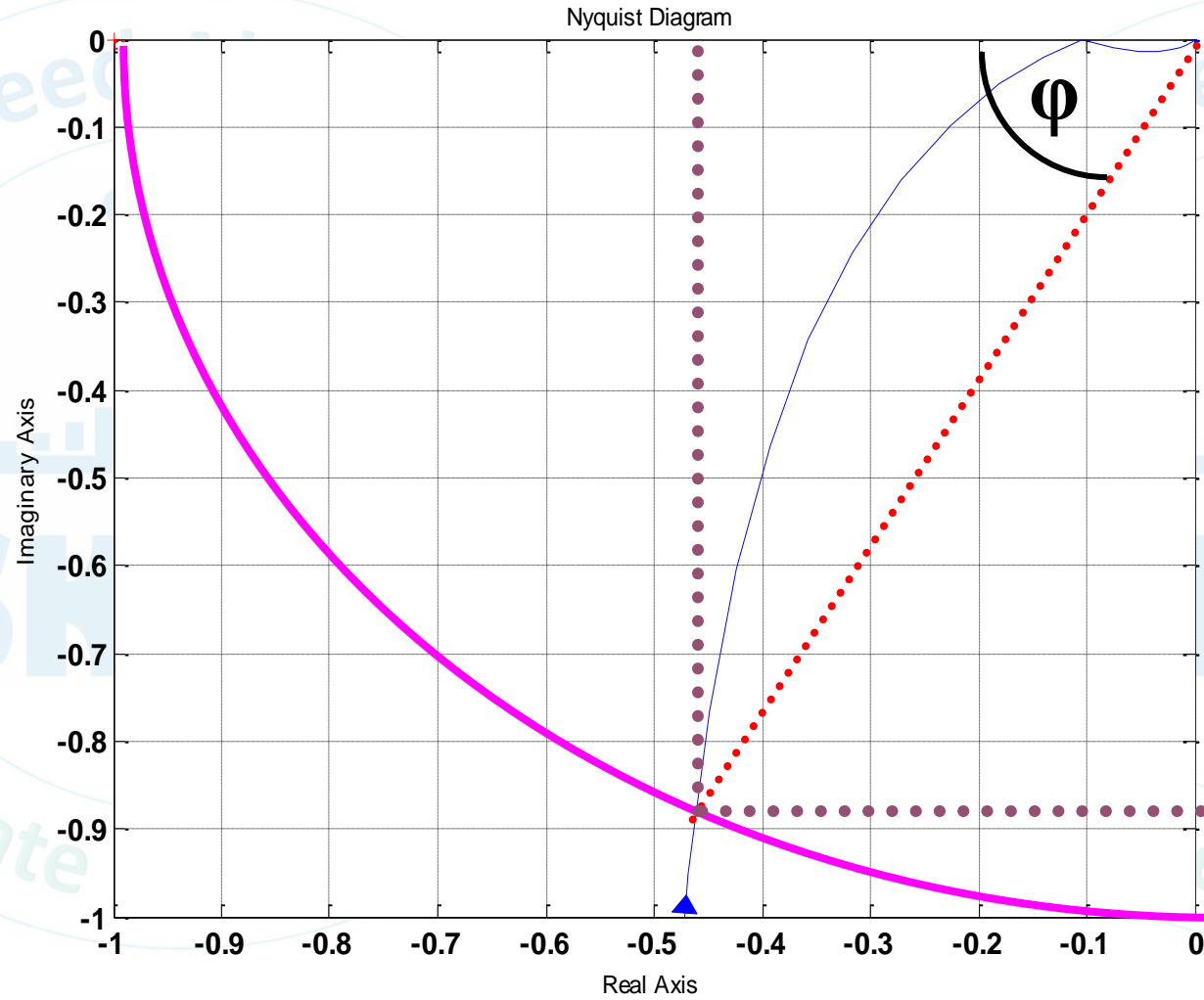
$$GM = 1/0.103 = 9.7$$





# Nyquist Stability

Example



$$\phi = \tan^{-1}(0.88/0.47)$$

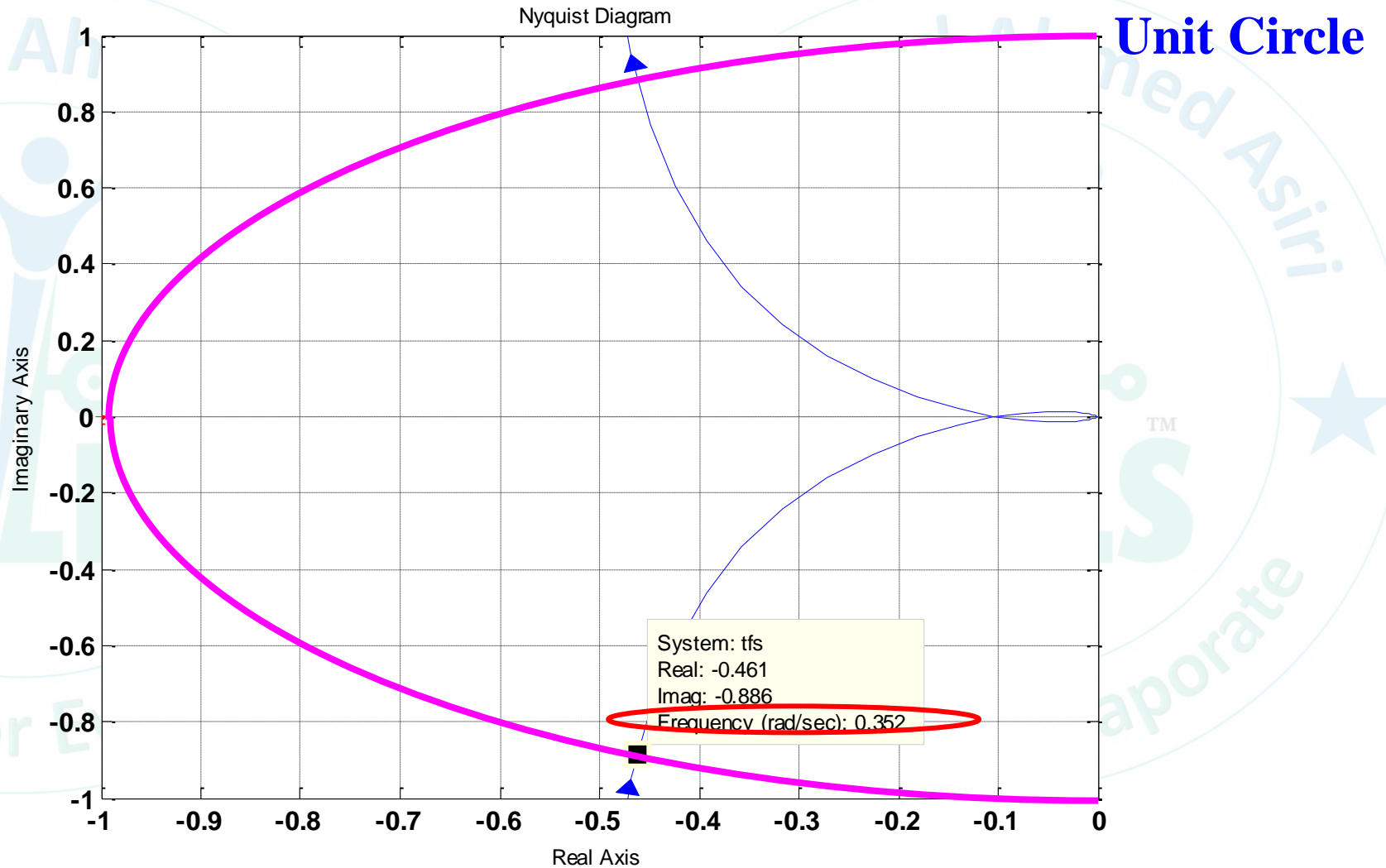
$$= 61.89^\circ$$

**Phase Margin**

$\phi = 61.89^\circ$

# Nyquist Stability

Example



# Nyquist Stability

## Example

```
>> [Gm,Pm,wg,wp]=margin(tfs)
```

```
Gm = 9.6456
```

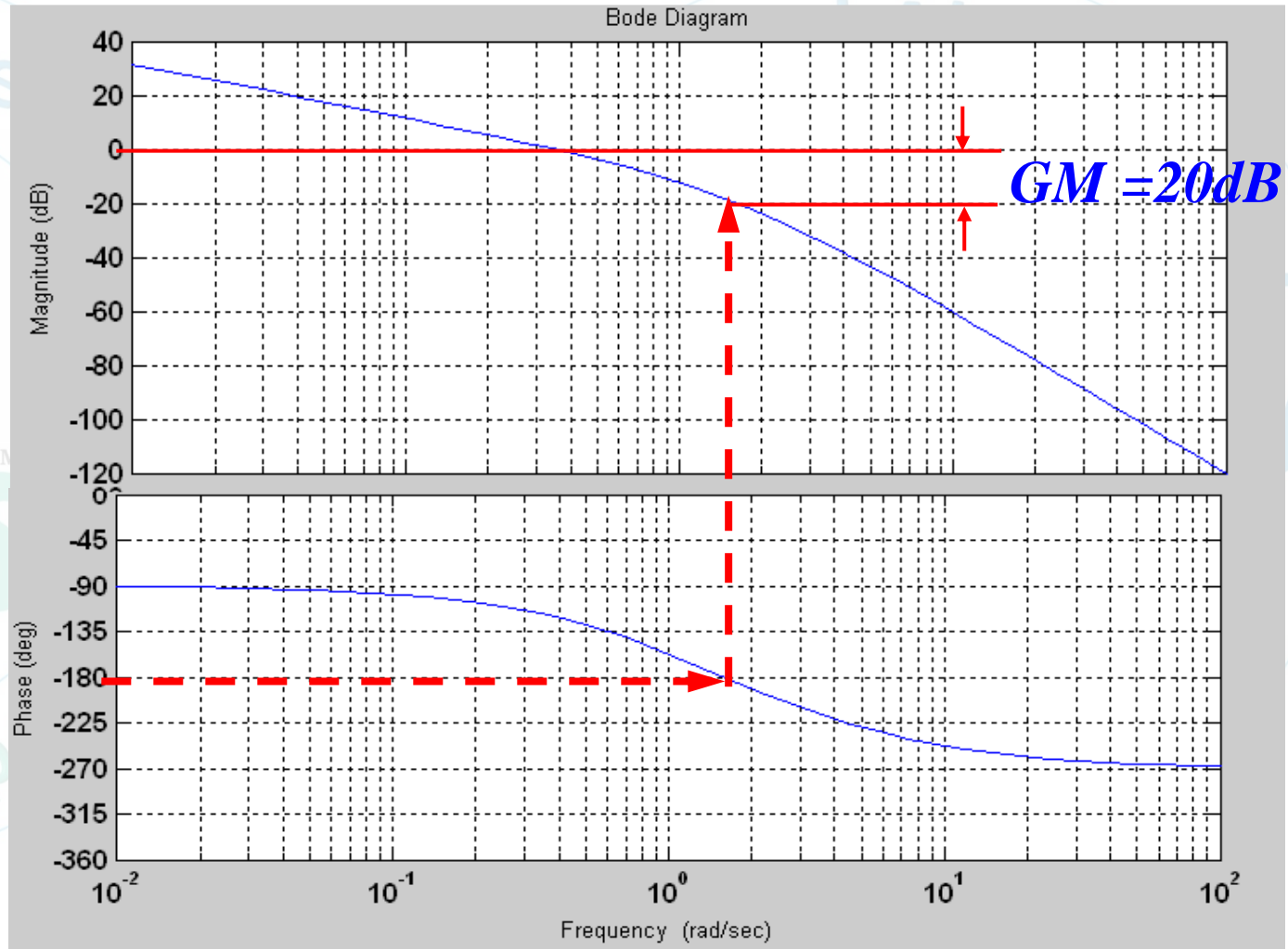
```
Pm = 62.4587
```

```
wg = 1.5877
```

```
wp = 0.3497
```

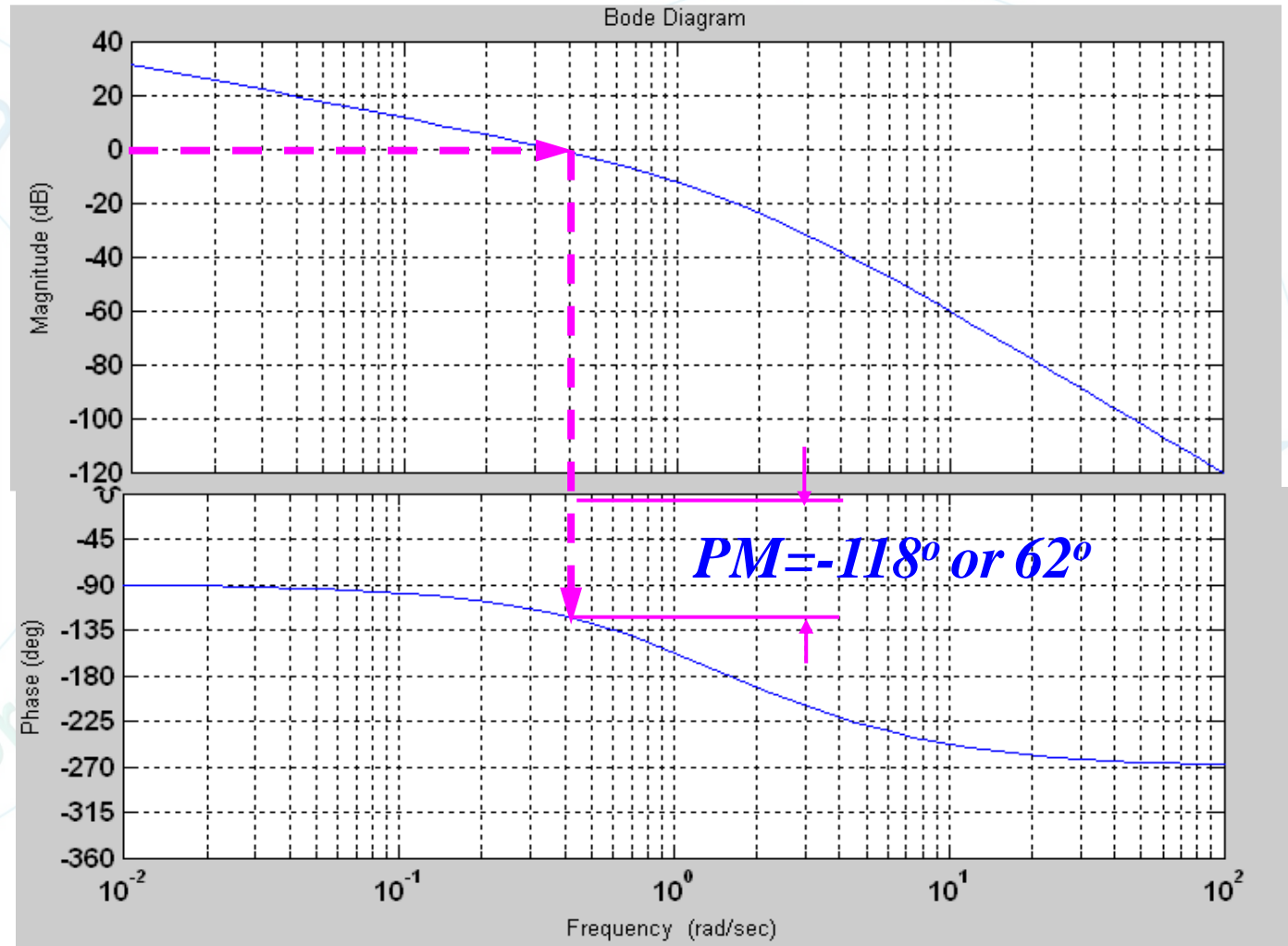
# Nyquist Stability

## Example



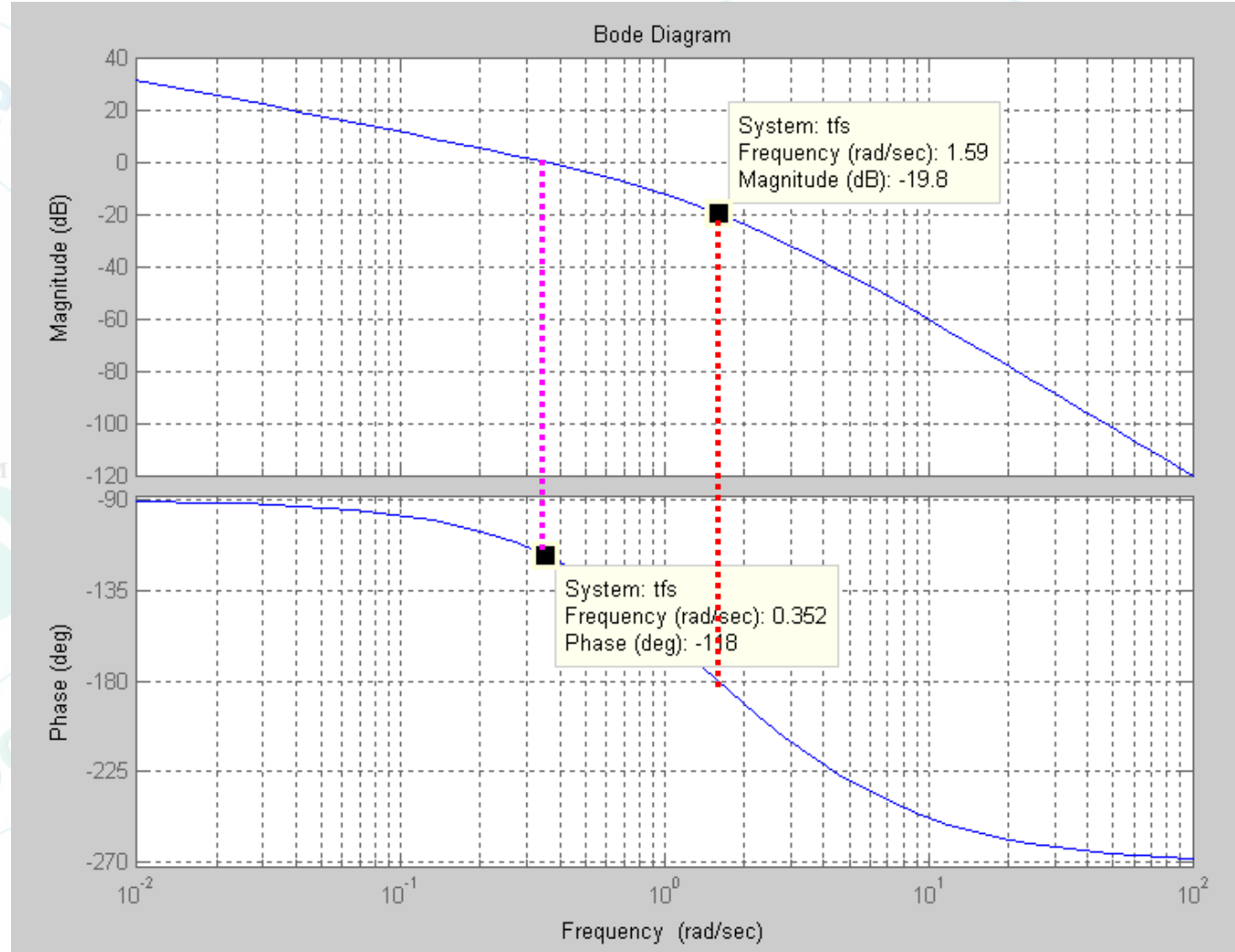
# Nyquist Stability

## Example



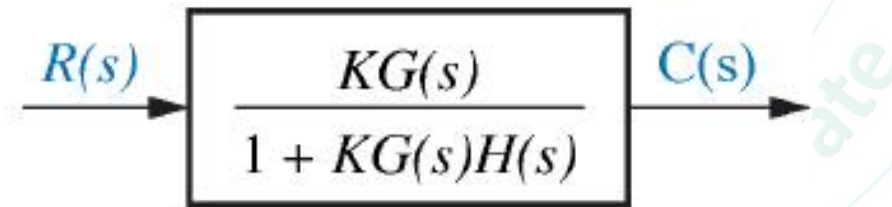
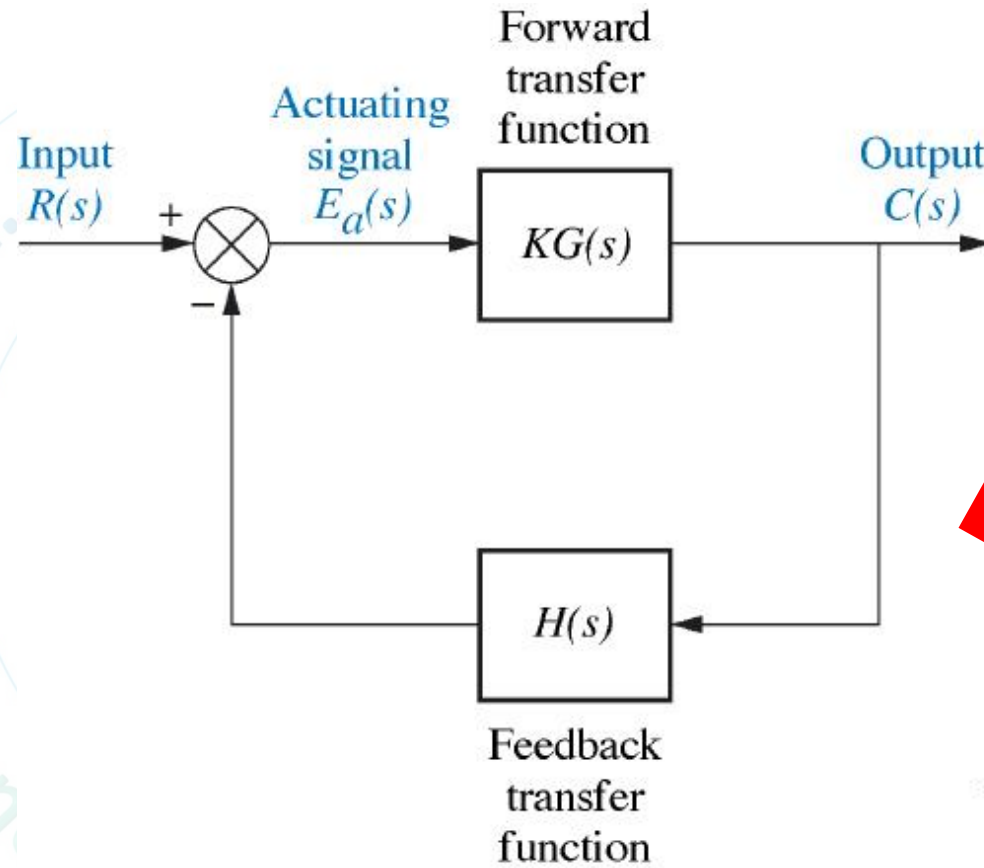
# Nyquist Stability

## Example





# Nyquist Stability





# Nyquist Stability

When  $1 + KG(s)H(s) = 0$

System output  $\rightarrow \infty$



**a. Magnitude Property**

$$KG(s)H(s) = -1,$$

or

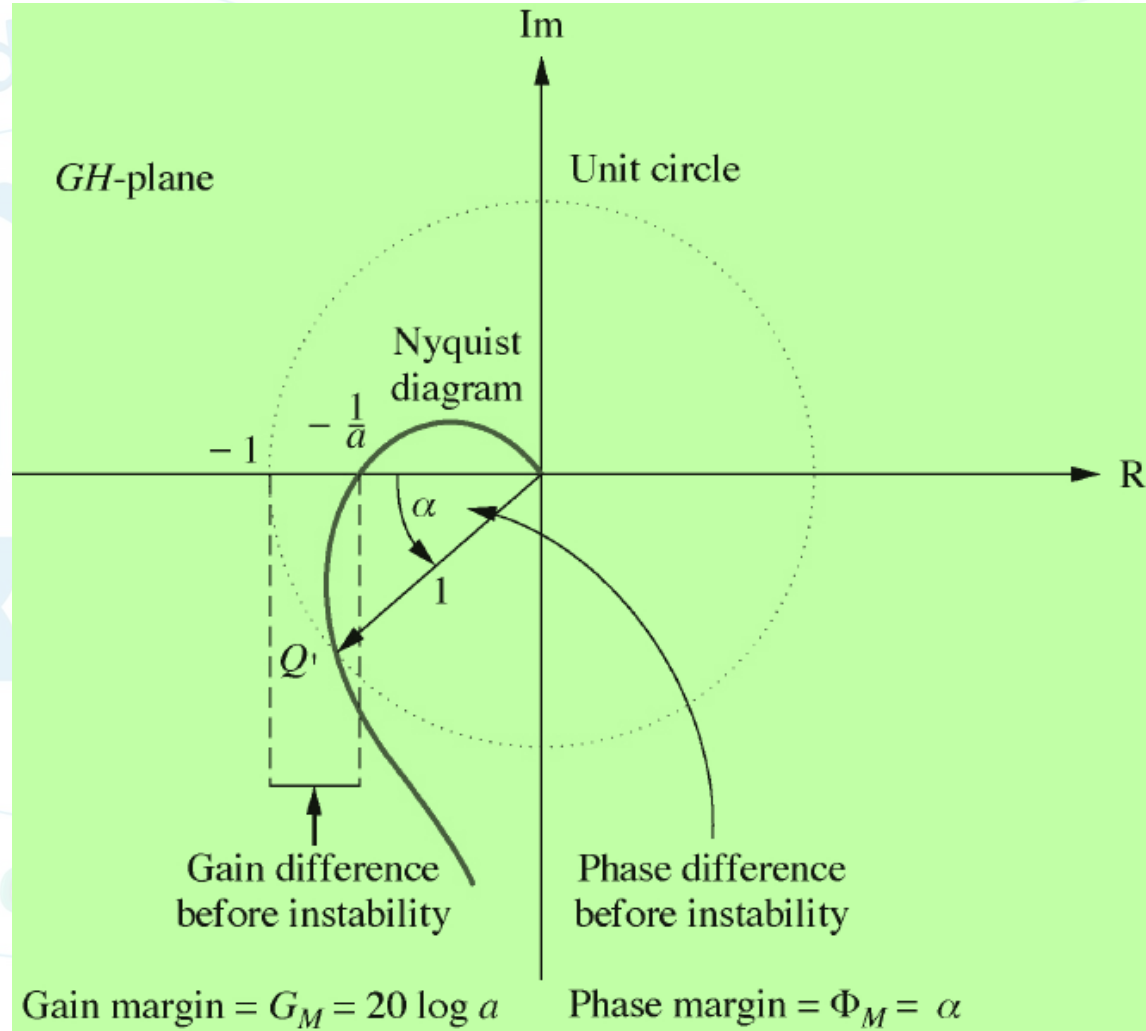
$$K = \frac{1}{|G(s)H(s)|}$$

**Gain Margin**

**b. Phase angle Property**

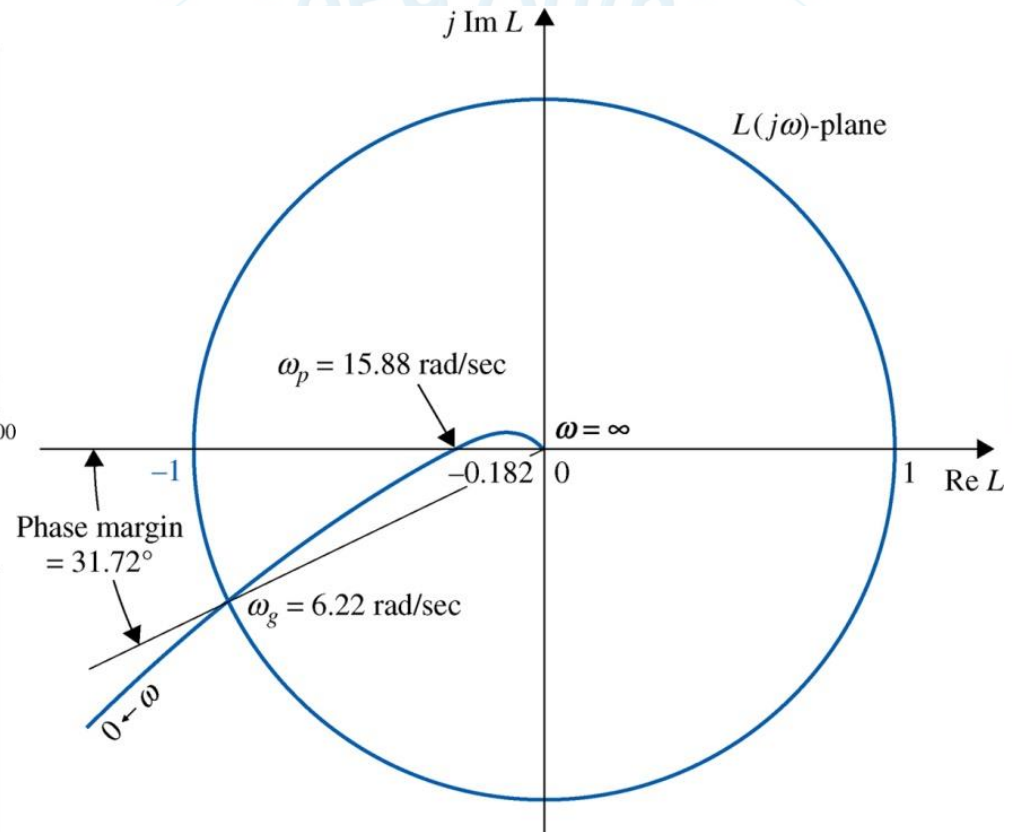
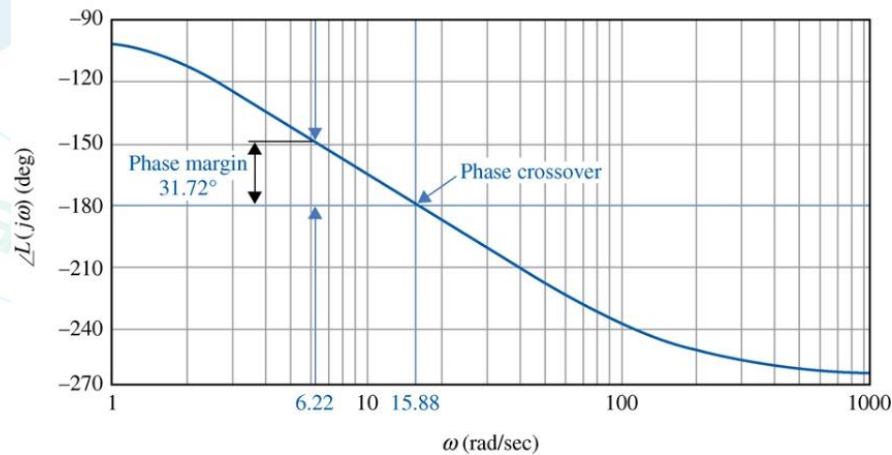
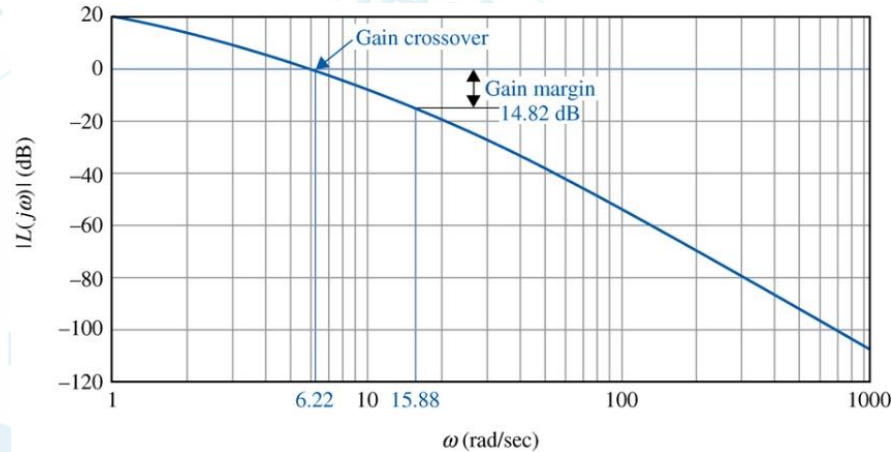
$$\angle [G(s)H(s)] = \pi$$

# Nyquist Stability



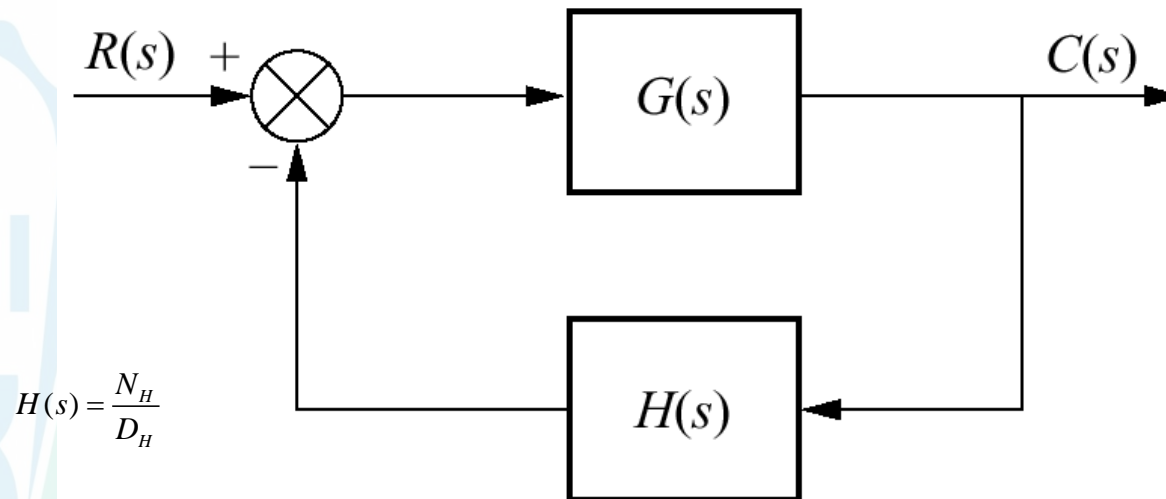
# Nyquist Stability

$$L(s) = \frac{2500}{s(s+5)(s+50)}$$

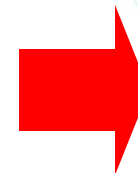


# Nyquist Stability

Defines number of closed-loop poles in the right half-plane

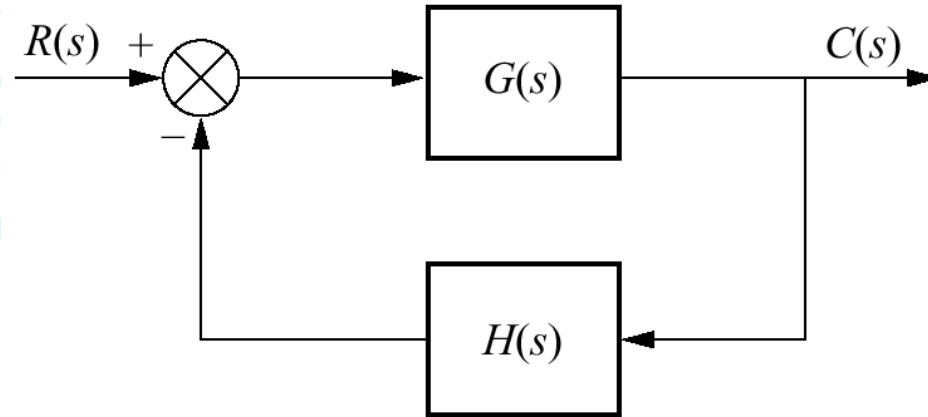


$$G(s) = \frac{N_G}{D_G} \quad \&$$

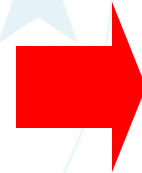


$$G(s)H(s) = \frac{N_G}{D_G} \frac{N_H}{D_H}$$

# Nyquist Stability



$$G(s)H(s) = \frac{N_G N_H}{D_G D_H}$$



$$1 + G(s)H(s) = \frac{N_G N_H + D_G D_H}{D_G D_H}$$



$$T(s) = \frac{G(s)}{1 + G(s)H(s)} = \frac{N_G D_H}{D_G D_H + N_G N_H}$$

# Nyquist Stability

## Relationships between:

Poles of  $1+G(s)H(s)$  & Poles of  $G(s)H(s)$

$$G(s)H(s) = \frac{N_G N_H}{D_G D_H}$$

$$1 + G(s)H(s) = \frac{N_G N_H + D_G D_H}{D_G D_H}$$

Zeros of  $1+G(s)H(s)$  & Poles of  $T(s)$

$$T(s) = \frac{G(s)}{1 + G(s)H(s)} = \frac{N_G D_H}{D_G D_H + N_G N_H}$$



# Nyquist Diagram and Analysis

## Nyquist Criterion

- Let us first introduce the most **important equation** when dealing with the Nyquist criterion:

$$Z = N + P$$

- Where:
  - **Z** is the number of zeros of the characteristic equation (and therefore the number of poles of the closed-loop transfer function) that are in the right-half of the  $s$  plane.
  - **N** is the number of encirclements of the  $(-1, 0)$  point.
  - **P** is the number of poles of the open-loop characteristic equation that are in the right-half of the  $s$  plane.



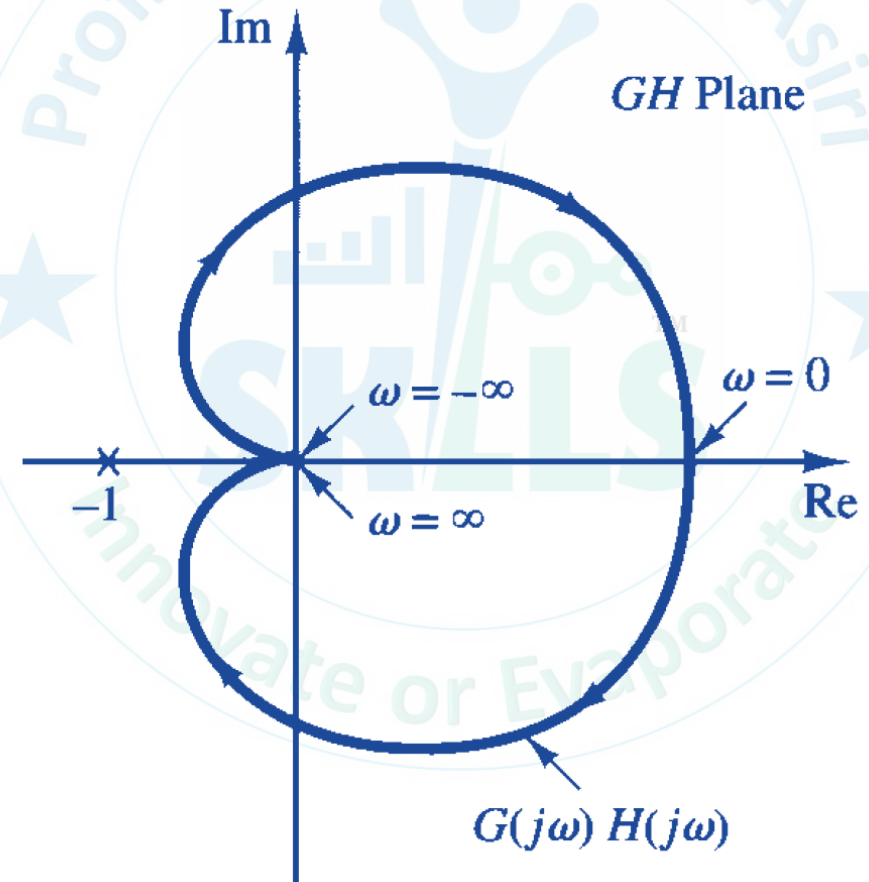
# Nyquist Diagram and Analysis

## Example

Investigate the stability of  $GH(s) = \frac{K}{(1+T_1s)(1+T_2s)}$  using Nyquist Stability Criteria

Since  $P = 0$ , so we need  $N=Z=0$  for stability.

As shown in the figure, there is no encirclement for  $-1$ . Hence, the closed loop system is stable for any positive value of  $K, T_1, T_2$

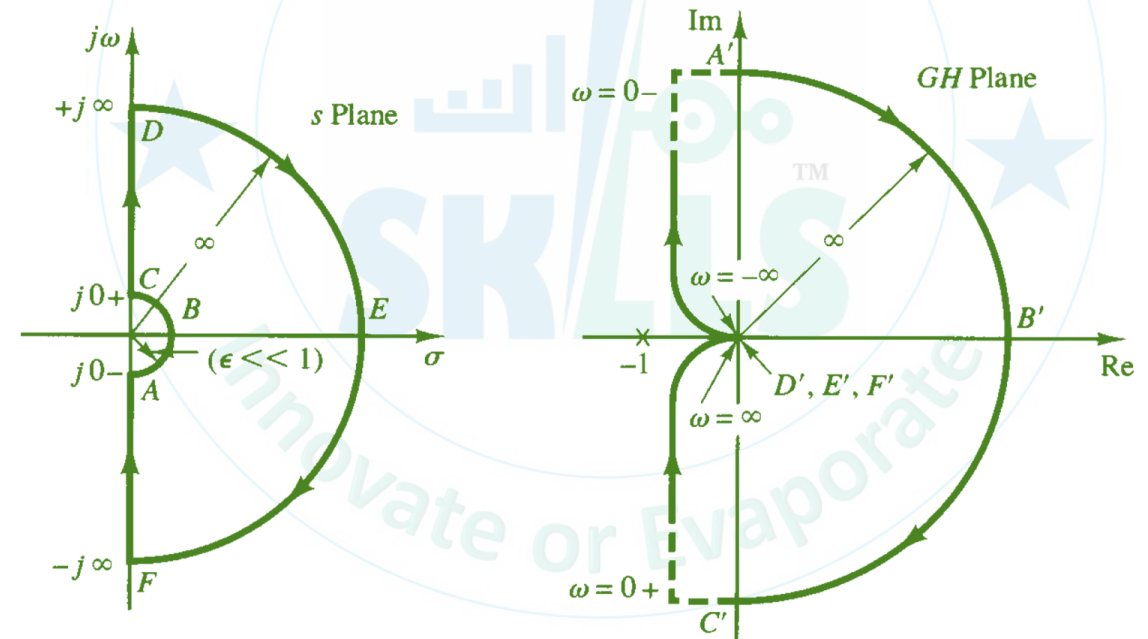


# Nyquist Diagram and Analysis

## Example

Investigate the stability of  $G(s) = K/[s(1 + Ts)]$  using Nyquist Stability Criteria

Since  $P = 0$ , so we need  $N=Z=0$  for stability.  
As shown in the figure, there is no encirclement for -1. Hence, the closed loop system is stable.



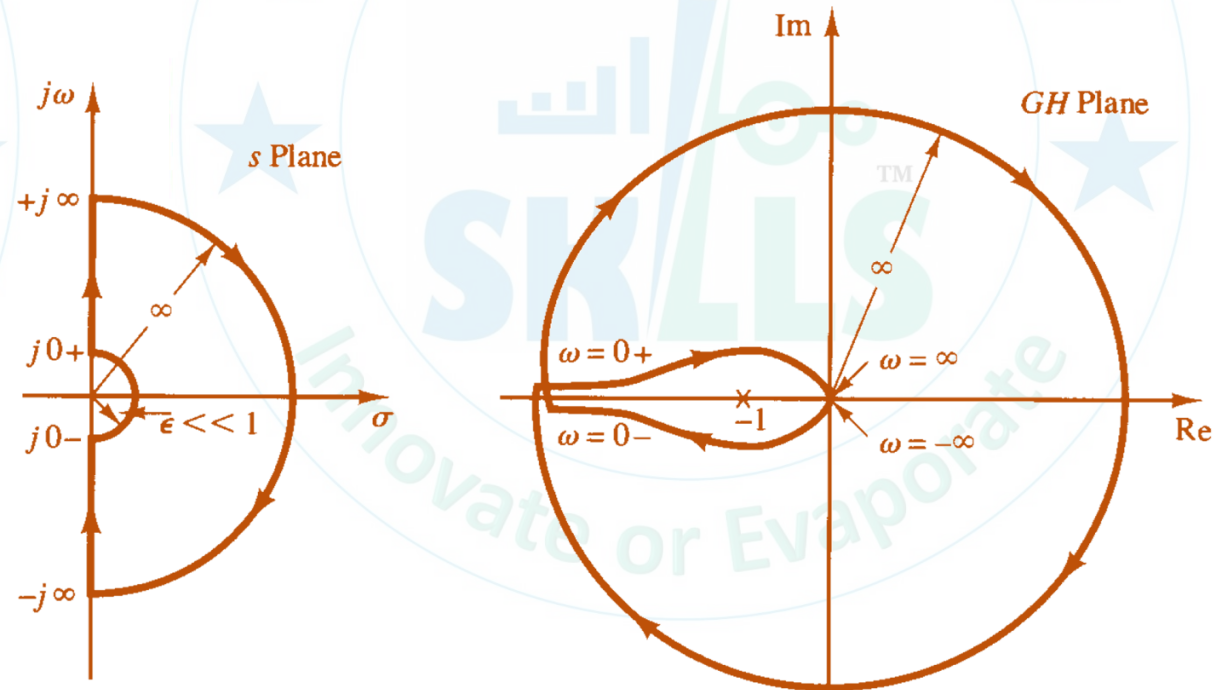
# Nyquist Diagram and Analysis

## Example

Investigate the stability of  $G(s) = K / [s^2 (1 + Ts)]$  using Nyquist Stability Criteria

Since  $P = 0$  for positive  $T$ , so we need  $N=Z=0$  for stability.

But as shown in the figure, there is two clockwise encirclements for  $-1$  so  $N = 2$ . Hence, the closed loop system is unstable.

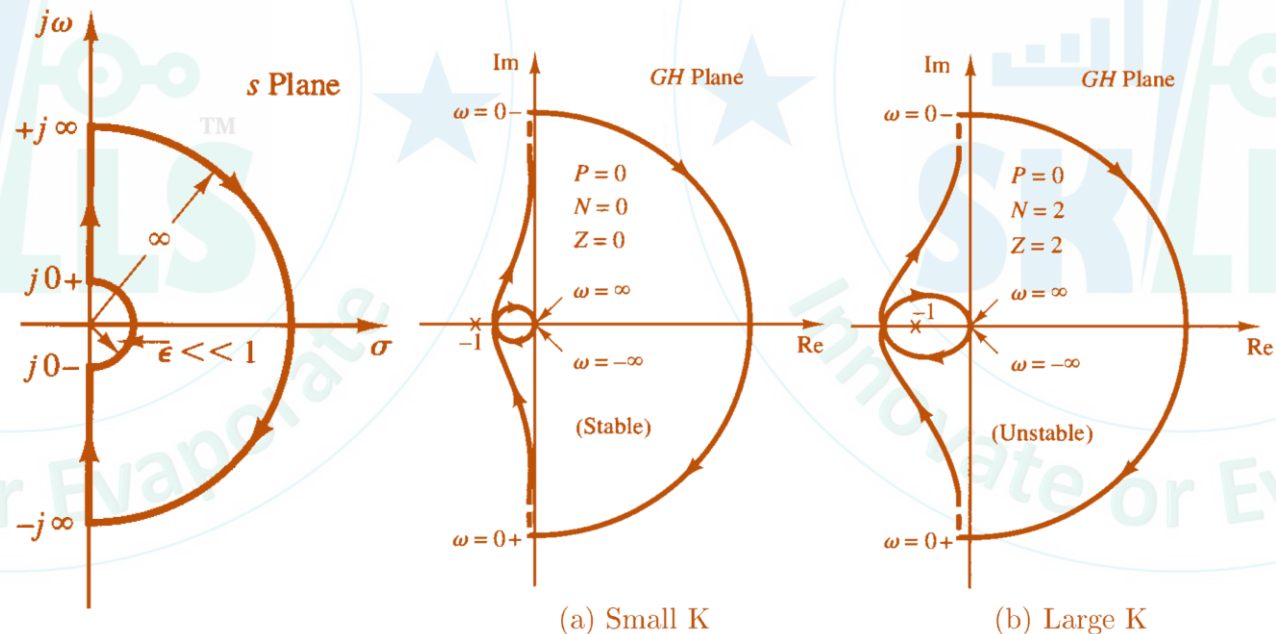


# Nyquist Diagram and Analysis

## Example

Investigate the stability of  $GH(s) = \frac{K}{s(1+T_1s)(1+T_2s)}$  using Nyquist Stability Criteria

Since  $P = 0$  for positive  $T_1$  and  $T_2$ , so we need  $N=Z=0$  for stability.



# Nyquist Diagram and Analysis

## Example

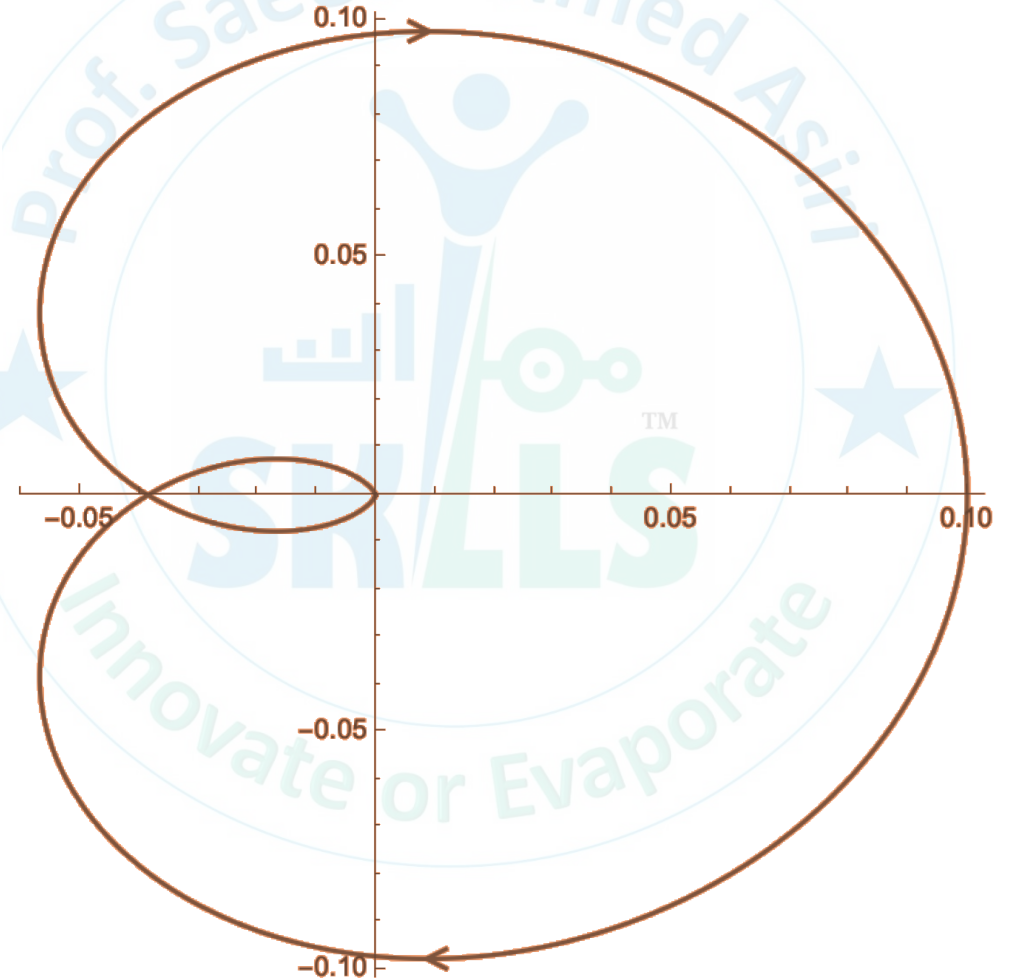
Consider the following system:

$$G(s) = \frac{1}{(s + 2)(s^2 + 2s + 5)}$$

Suppose this is in unity feedback with a constant gain controller  $K$ . In other words, we have a negative feedback loop where the forward gain is  $KG(s)$  and the loop gain is also  $KG(s)$ .

Investigate the stability of the system using

- Routh Array
- Nyquist Plot







**END**